

Eclipse Opening Roof Design Worksheet

This worksheet is a summary of design calculations from the Eclipse Opening Roof Design Manual
October 2013

Owners: EILEEN CLARK Address: 270 DOWLING STREET DUNGOO
1. Wind Design Factors

Wind Region = A

Terrain Category = 2

Shielded or Non-shielded = NONSHIELDED

2. Design Wind Pressure, q_z

Using the Design Wind Factors select q_z from the Tables in Section 2 of Design Manual. $q_z = \underline{1.02}$ kPa

3. Pressure Coefficient, C_{p_u} & C_{p_d}

Determine both UPWARD and DOWNWARD pressure coefficients.

Height of Structure $h_o = \underline{3.5}$ m $h_o/w_o = \underline{0.827}$ $C_{p_u} = \underline{1.2}$
Height of Building $h = \underline{3.5}$ m
Projection of Structure $w_o = \underline{4.05}$ m $h_o/h = \underline{1.0}$ $C_{p_d} = \underline{0.6}$
Number of Enclosed Sides = 3

4. Wind Pressure (kPa)

Calculate wind pressure for both UPWARD and DOWNWARD directions.

Upward Pressure $P_u = q_z \times C_{p_u} = \underline{1.02} \times \underline{1.2}$ $P_u = \underline{1.224}$ kPa
Downward Pressure $P_d = q_z \times C_{p_d} = \underline{1.02} \times \underline{0.6}$ $P_d = \underline{0.612}$ kPa

5. Select Louvre Span (m)

Using P_u and P_d select the maximum louvre span from the Tables in Section 5 of the Design Manual.

Maximum Louvre Span, based on UPWARD pressure = 3.2 m

Maximum Louvre Span, based on DOWNWARD pressure = 4.2 m

The Allowable Maximum Span is the LESSER of these two values.

Maximum Louvre Span, $L_s = \underline{3.2}$ m

6. Louvre Support Beams

Calculate the Uniformly Distributed Beam Load (UDL) then select beam with appropriate span from Table 6.1.

For Design Pressure, P use the HIGHER value of P_u and P_d $P = \underline{1.224}$ kPa

EDGE BEAM Louvre Span Length (dist. between tracks): $L = \underline{3.2}$ m.
 $UDL = P \times L/2 = \underline{1.224} \times \underline{1.6}$ $UDL = \underline{1.958}$ kN/m

MID BEAM Louvre Span Lengths (dist. between tracks): $L1 = \underline{\quad}$ m $L2 = \underline{\quad}$ m
 $UDL = P \times (L1 + L2)/2 = \underline{\quad} \times \underline{\quad}$ $UDL = \underline{\quad}$ kN/m

Beam Selection Summary:

	<u>UDL</u>	<u>Size</u>	<u>Max. Span</u>
Beam 1	<u>1.958</u>	<u>250x50x3</u>	<u>5.39</u>
Beam 2			
Beam 3			

SHADEMASTER SHELTER SYSTEM

Design Sheet – Roof System

Calculations and tables are referenced from the SHADEMASTER Shelter System Simplified Design Procedures Manual June

Client: EILEEN CLARK BANK HOTEL.

Designed by: HV ALUMINIUM

Address: 270 DOWLING STREET, DUNGOG

Date: 27.11.24

REGION	A
TC	2
NON SHIELDED	
qz=	0.835 kPa
ATTACHED	
c	Cp= 1.06

AUSTRALIAN WIND REGION

TERRAIN CATEGORY CLASSIFICATION

SHIELDING CLASSIFICATION (Shielded, Partially Shielded, Non-Shielded)

ULTIMATE WIND PRESSURE (selected from Table U1) $R = h + P$

STRUCTURE TYPE (Attached or Freestanding / Flat Roof) = 0.65

COEFFICIENT OF PRESSURE (selected from 6 conditions Page 12 to 14)
 $p = (qz) \times (Cp) =$ kPa

OR With Naturelite $p = (qz) \times (Cp) \times 1.1^* =$ kPa

*Maximum One Naturelite per Metre or + Naturelite at 600mm spacing use 1.333

ROOFING DESIGN

P=	0.885 kPa
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ROOF DESIGN PRESSURE

ROOF SHEET TYPE: 90
INSULATED

ROOF SHEET SUPPORT CONDITION	READ FROM TABLE		
	Region A	Region B	Region C
☒ Simply Supported	Table RS/A	Table RS/B	Table RS/C
☐ Single Cantilever	Table RS/A	Table RS/B	Table RS/C
☐ Continuous Spans	Table RS/A	Table RS/B	Table RS/C

Ls=	5.0 m
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ACTUAL ROOF SPAN REQUIRED: 5.0 metres MAXIMUM SPAN PERMITTED: 5.68 metres

BEAM DESIGN

Wb=	2.09 kN/m
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Calculate Load on Beam $Wb = \frac{.835 \times 1.06 \times 3.8 \times .616}{(qz)(Cp)(Ls)(r)} = 2.09$ (kN/m)

BEAM TYPE: DOUBLE
250x50x3
ALUMINIUM

BEAM SUPPORT CONDITION	READ FROM TABLE
☒ Simply Supported	Region A, B or C
☐ Single Cantilever	Region A, B or C
☐ Double Cantilever	Region A, B or C
☐ Continuous Spans	Region A, B or C

Lb=	6.7 m
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ACTUAL BEAM SPAN REQUIRED 6.7 metres MAXIMUM SPAN PERMITTED: 6.9 metres

PL=	kN
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POST & FOOTING DESIGN

Calculate Load on Post $PL =$

$(qz) \times (Cp) \times (Ls) \times (Lb) \times (k) \times (r) =$ (kN)

(k) = Post Load Coefficient
- refer Table A2
(r) = Beam Load Factor
- refer Table A1
(d) = Lateral Load Factor
- refer Table A3

POST LOAD

Use Post Type = x x (Attached structure only)

Select Post & Footing from Table P1 or P2

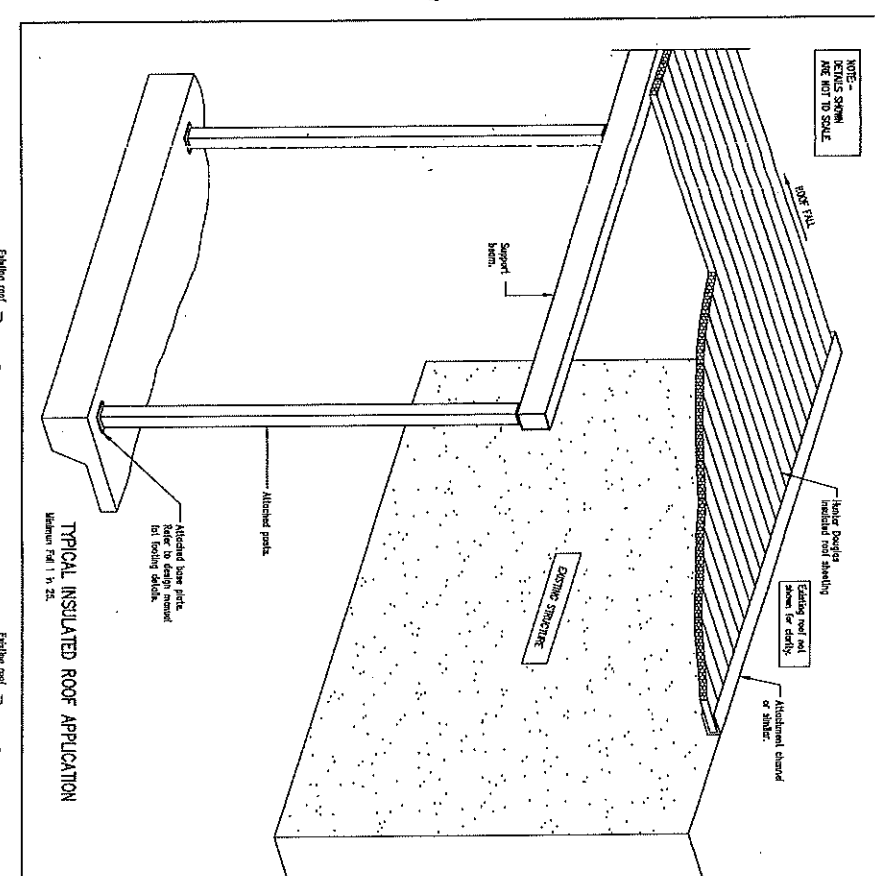
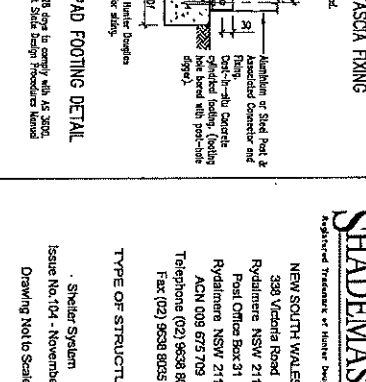
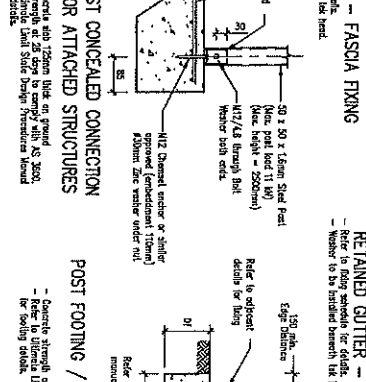
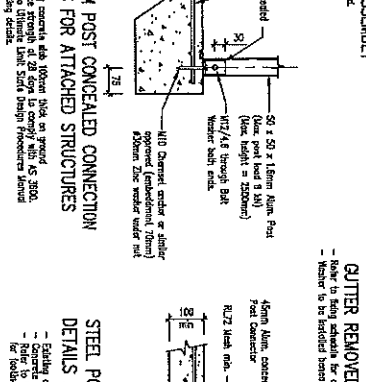
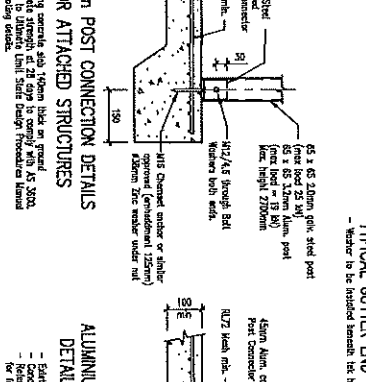
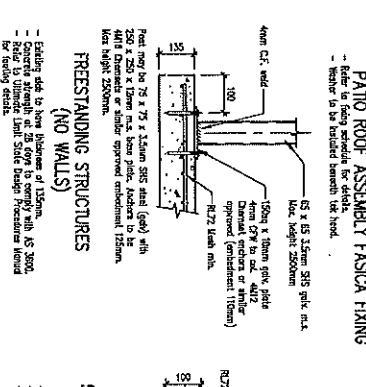
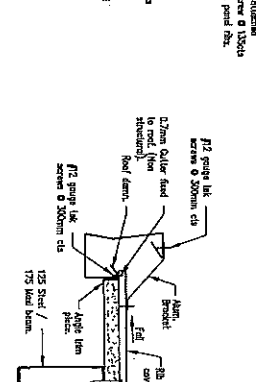
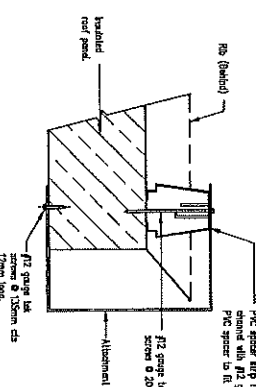
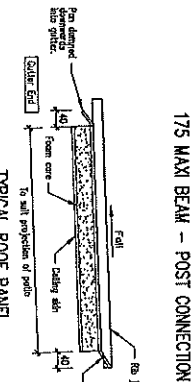
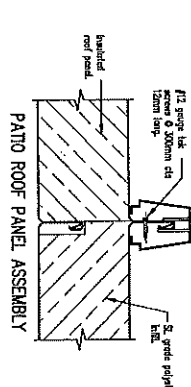
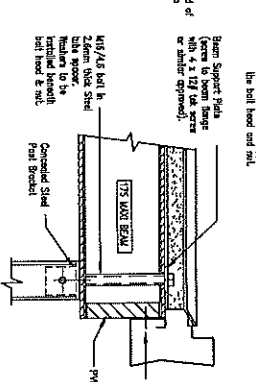
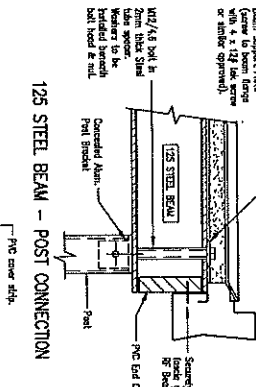
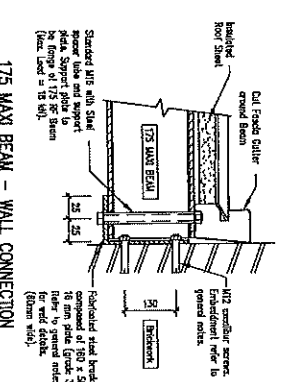
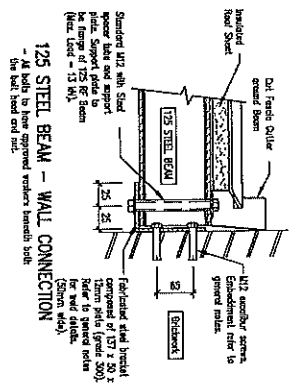
Footing size = x x
OR
100mm Slab = (m²)

Calculate Lateral Post Loads For Freestanding Structures

$F1 = \frac{(Lb \times k + 3.2)}{(qz)(Ls)(r)} =$ kN

$F2 = \frac{(Ls \times r + d)}{(qz)(Lb)(k)} =$ kN

SELECT THE GREATER VALUE OF F1 AND F2 POST SIZE FOR FREESTANDING STRUCTURE



MAJOR STRUCTURAL COMPONENT SPECIFICATION	
ROOF PANEL	55mm cold rolled steel with 5mm thick protective zinc plating.
FASCIA GUTTER	40mm x 100mm x 10mm steel.
125 STEEL BEAM	125 x 125 x 125 steel (2 thicknesses "C" section).
175 MAXI BEAM	175 x 175 x 175 steel (2 thicknesses "C" section).
POSTS	55 x 55 x 55 steel (2 thicknesses "C" section).
POST CONNECTOR (45mm)	55mm x 55mm x 55mm steel (2 thicknesses "C" section).
POST CONNECTOR (55mm)	55mm x 55mm x 55mm steel (2 thicknesses "C" section).

SHADEMASTER
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SHELTER SYSTEM DESIGNED AND TESTED BY

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Drawing Not to Scale